

## General Information

- Please add the *initial of your first name* and *your surname* + "\_" in the beginning of each file name. For example, if your name is John Smith, a file *fig1\_1-01.eps* should be *jsmith\_fig1\_1-01.eps*
- Please archive all of your figure files and integral data files for all cases into one zipped file. The file name should be *your first name initial* and *your surname* + ".zip". For example, if your name is John Smith, the file name is *jsmith.zip* .
- The archived file should be uploaded to the FTP server of NMRI via FTP. User account name and password are required to login the server. Please contact the organizer ( [cfdws05@nmri.go.jp](mailto:cfdws05@nmri.go.jp) ) to obtain these informations.

## Integral variables

### Coefficients of forces and moments

File name	int3.dat
Style	plain text

The data should be written as following format.

The items which are not available should be left blank.

```

beta = 0
CX = value
CXP = value
CXF = value
CY = value
CYP = value
CYF = value
CN = value
beta = 3
CX = value
CXP = value
CXF = value
CY = value
CYP = value
CYF = value
CN = value
beta = 6
CX = value
CXP = value
CXF = value
CY = value
CYP = value
CYF = value
CN = value
beta = 9
CX = value
CXP = value
CXF = value
CY = value
CYP = value
CYF = value
CN = value
beta = 12
CX = value

```

CXP = *value*  
 CXF = *value*  
 CY = *value*  
 CYP = *value*  
 CYF = *value*  
 CN = *value*

### Uncertainty analysis of coefficients of forces and moments

File name	int3ua.dat
Style	plain text

The data should be written as following format.  
 The items which are not available should be left blank.

beta = 0  
 ( E of CX )/(measured CX) = *value*  
 ( UV of CX )/(measured CX) = *value*  
 (-UV of CX )/(measured CX) = *value*  
 ( E of CY )/(measured CY) = *value*  
 ( UV of CY )/(measured CY) = *value*  
 (-UV of CY )/(measured CY) = *value*  
 ( E of CN )/(measured CN) = *value*  
 ( UV of CN )/(measured CN) = *value*  
 (-UV of CN )/(measured CN) = *value*  
 ( E of N/Y)/(measured N/Y) = *value*  
 ( UV of N/Y)/(measured N/Y) = *value*  
 (-UV of N/Y)/(measured N/Y) = *value*  
 beta = 3  
 ( E of CX )/(measured CX) = *value*  
 ( UV of CX )/(measured CX) = *value*  
 (-UV of CX )/(measured CX) = *value*  
 ( E of CY )/(measured CY) = *value*  
 ( UV of CY )/(measured CY) = *value*  
 (-UV of CY )/(measured CY) = *value*  
 ( E of CN )/(measured CN) = *value*  
 ( UV of CN )/(measured CN) = *value*  
 (-UV of CN )/(measured CN) = *value*  
 ( E of N/Y)/(measured N/Y) = *value*  
 ( UV of N/Y)/(measured N/Y) = *value*  
 (-UV of N/Y)/(measured N/Y) = *value*  
 beta = 6  
 ( E of CX )/(measured CX) = *value*  
 ( UV of CX )/(measured CX) = *value*  
 (-UV of CX )/(measured CX) = *value*  
 ( E of CY )/(measured CY) = *value*  
 ( UV of CY )/(measured CY) = *value*  
 (-UV of CY )/(measured CY) = *value*  
 ( E of CN )/(measured CN) = *value*  
 ( UV of CN )/(measured CN) = *value*  
 (-UV of CN )/(measured CN) = *value*  
 ( E of N/Y)/(measured N/Y) = *value*  
 ( UV of N/Y)/(measured N/Y) = *value*  
 (-UV of N/Y)/(measured N/Y) = *value*  
 beta = 9  
 ( E of CX )/(measured CX) = *value*  
 ( UV of CX )/(measured CX) = *value*  
 (-UV of CX )/(measured CX) = *value*

( E of CY )/(measured CY) = *value*  
( UV of CY )/(measured CY) = *value*  
(-UV of CY )/(measured CY) = *value*  
( E of CN )/(measured CN) = *value*  
( UV of CN )/(measured CN) = *value*  
(-UV of CN )/(measured CN) = *value*  
( E of N/Y )/(measured N/Y) = *value*  
( UV of N/Y )/(measured N/Y) = *value*  
(-UV of N/Y )/(measured N/Y) = *value*  
beta = 12  
( E of CX )/(measured CX) = *value*  
( UV of CX )/(measured CX) = *value*  
(-UV of CX )/(measured CX) = *value*  
( E of CY )/(measured CY) = *value*  
( UV of CY )/(measured CY) = *value*  
(-UV of CY )/(measured CY) = *value*  
( E of CN )/(measured CN) = *value*  
( UV of CN )/(measured CN) = *value*  
(-UV of CN )/(measured CN) = *value*  
( E of N/Y )/(measured N/Y) = *value*  
( UV of N/Y )/(measured N/Y) = *value*  
(-UV of N/Y )/(measured N/Y) = *value*

**Fig.3-1 Integral variables: Coefficients of forces and moments,  
 $C_X, C_Y, C_N, N/Y$  versus  $\beta$**

File name	fig3-01_CX.eps (for $C_X$ ) fig3-01_CY.eps (for $C_Y$ ) fig3-01_CN.eps (for $C_N$ ) fig3-01_NY.eps (for $N/Y$ )
Axis size	75 [mm] $\times$ 40 [mm]
Horizontal-axis variable and range	$-3 \leq \beta \leq 15$
Vertical-axis variable and range	$-0.025 \leq C_X \leq 0.0$ $-0.02 \leq C_Y \leq 0.1$ $-0.005 \leq C_N \leq 0.035$ $0.0 \leq N/Y \leq 0.7$
Style	CFD solid line, EFD open circles

Red line is corrected at 06/Dec/2004

Magenta line is corrected at 20/Dec/2004

**Fig.3-2 Uncertainty analysis of coefficients of forces and moments  
 $C_X, C_Y, C_N, N/Y$  versus  $\beta$**

This figure will be made by NMRI, since it is difficult to determine the ranges for  $E$  and  $\pm U_V$  in advance. Please send us the data file "int3ua.dat" described above.  $E$  and  $U_V$  should be divided by the corresponding measured data, e.g.  $E/(\text{measured } C_X)$ ,  $U_V/(\text{measured } C_Y)$  and so on. (10/Dec/2004)

**Fig.3-3 Axial velocity contours and cross flow vectors  
on the WAKE 1 plane (  $\beta = 0, 6, 12[\text{deg}]$  )**

File name	fig3-03_00_wake.eps ( $\beta = 0^\circ$ , $u/U$ contours ) fig3-03_06_wake.eps ( $\beta = 6^\circ$ , $u/U$ contours ) fig3-03_12_wake.eps ( $\beta = 12^\circ$ , $u/U$ contours ) fig3-03_00_vw.eps ( $\beta = 0^\circ$ , $v/U, w/U$ vectors ) fig3-03_06_vw.eps ( $\beta = 6^\circ$ , $v/U, w/U$ vectors ) fig3-03_12_vw.eps ( $\beta = 12^\circ$ , $v/U, w/U$ vectors )
Axis size	160 [mm] $\times$ 40 [mm]
Horizontal-axis variable and range	$-0.16 \leq y/L_{PP} \leq 0.16$
Vertical-axis variable and range	$-0.08 \leq z/L_{PP} \leq 0.0$
Contour range and levels	$0 \leq u/U \leq 1$ , $\Delta(u/U) = 0.1$
Reference vector	magnitude 0.1 corresponds to 2 [mm]
Style	$u/U$ contours: solid lines

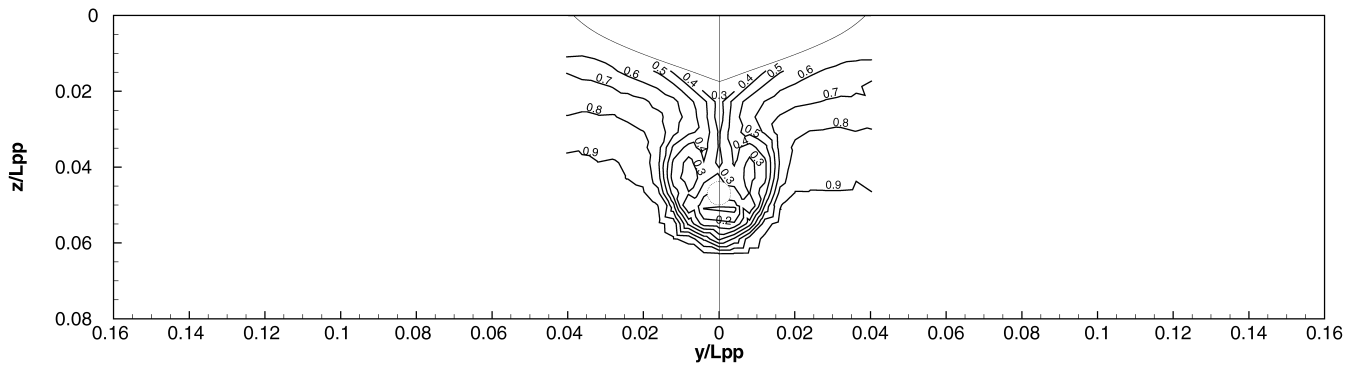


Fig. 3- 1: fig3-03\_00\_wake.eps

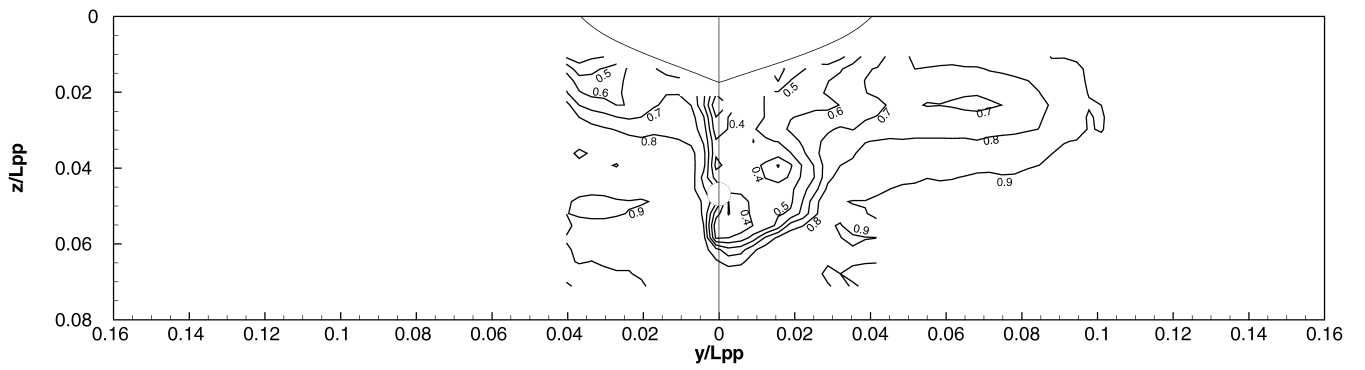


Fig. 3- 2: fig3-03\_06\_wake.eps

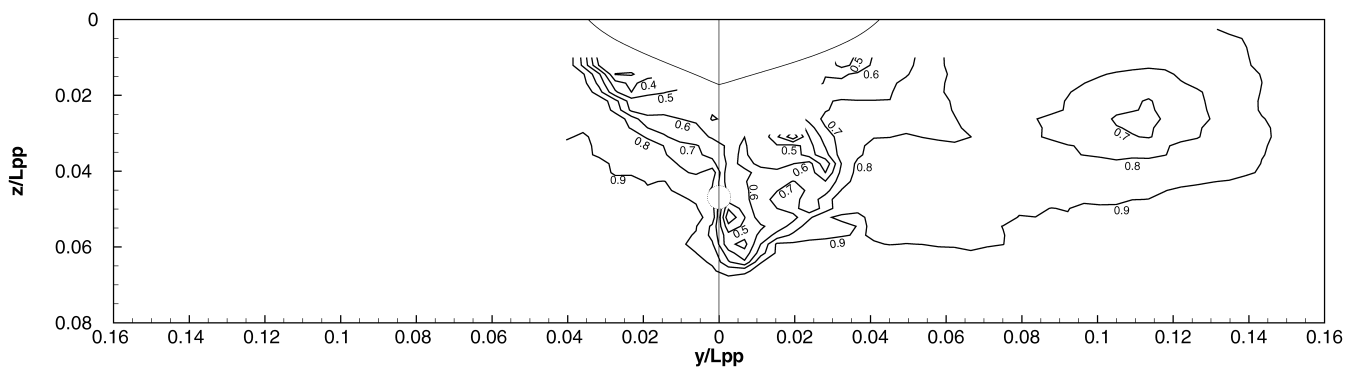


Fig. 3- 3: fig3-03\_12\_wake.eps

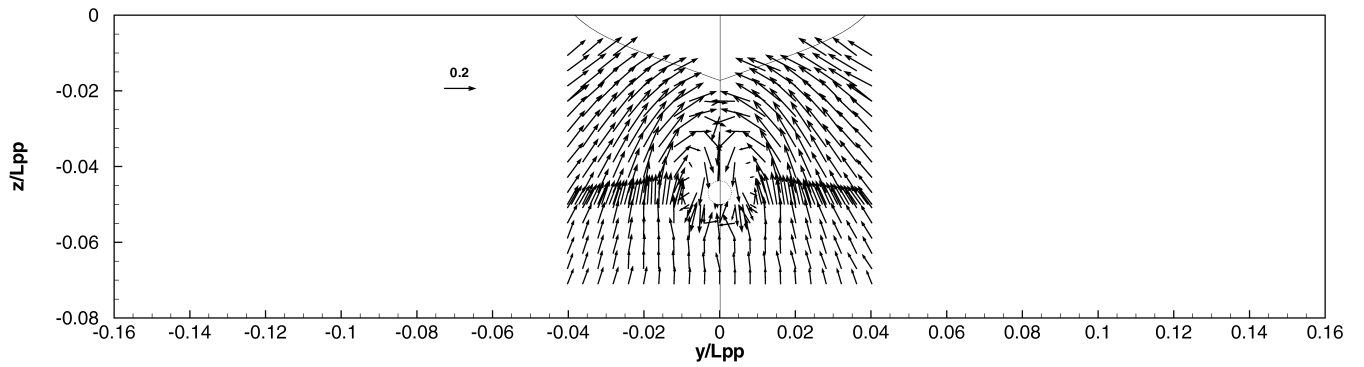


Fig. 3- 4: fig3-03\_00\_vw.eps

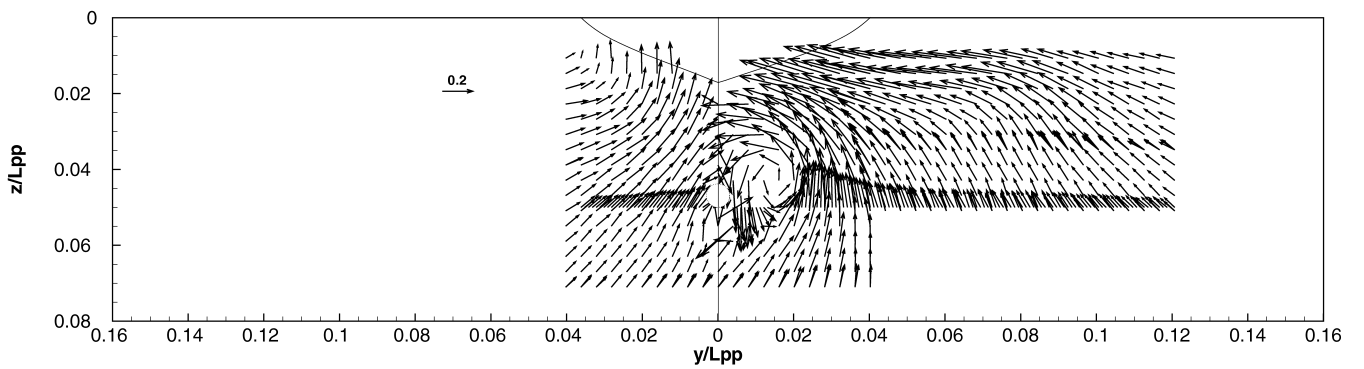


Fig. 3- 5: fig3-03\_06\_vw.eps

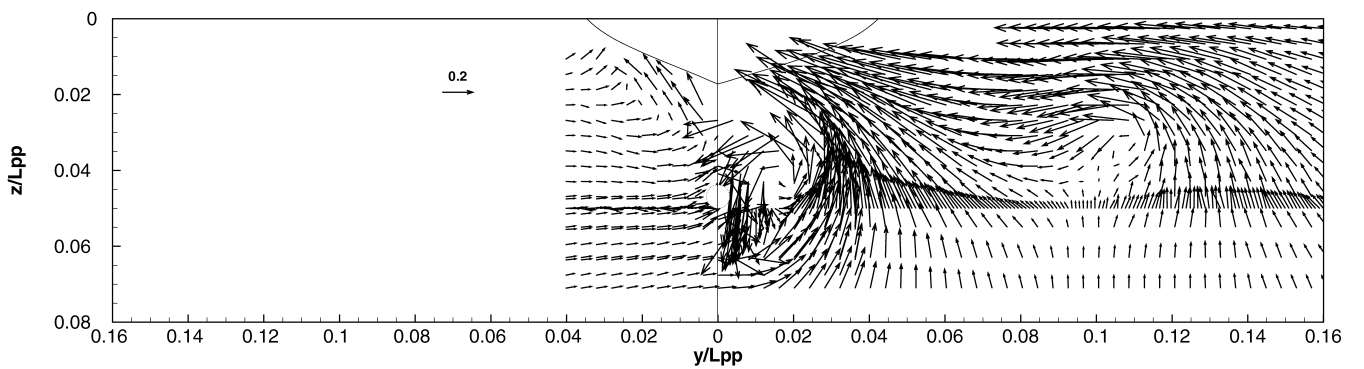


Fig. 3- 6: fig3-03\_12\_vw.eps

**Fig.3-4 Velocity on the WAKE 1 plane at  $z/L_{PP} = -0.05$ ,  $\beta = 0, 6, 12[deg]$** 

File name	fig3-04_00.eps ( $\beta = 0^\circ$ ) fig3-04_06.eps ( $\beta = 6^\circ$ ) fig3-04_12.eps ( $\beta = 12^\circ$ )
Axis size	75 [mm] $\times$ 40 [mm]
Horizontal-axis variable and range	$-0.05 \leq y/L_{PP} \leq 0.18$
Vertical-axis variable and range	$-0.6 \leq u/U, v/U, w/U \leq 1.0$
Style	$u/U$ : CFD solid line; EFD open squares $v/U$ : CFD dashed line; EFD open triangles $w/U$ : CFD dotted line; EFD open circles

Red line is corrected at 10/Dec/2004

**Fig.3-5 Uncertainty analysis of velocity on the WAKE 1 plane at  $z/L_{PP} = -0.05$ ,  $\beta = 0, 6, 12[deg]$** 

File name	fig3-05_00.eps ( $\beta = 0^\circ$ ) fig3-05_06.eps ( $\beta = 6^\circ$ ) fig3-05_12.eps ( $\beta = 12^\circ$ )
Axis size	80 [mm] $\times$ 60 [mm]
Horizontal-axis variable and range	$-0.16 \leq y/L_{PP} \leq 0.16$
Vertical-axis variable and range	$-0.1 \leq E/U, \pm U_V/U \leq 0.1$
Style	$u/U$ : E solid line; $U_V$ dashed line $v/U$ : E dash dot line; $U_V$ dotted line $w/U$ : E long dashed line; $U_V$ dash double dot line

Red line is corrected at 03/Dec/2004

**Fig.3-6 Kinematic eddy viscosity ( $\nu_t$ ) and longitudinal component of vorticity ( $\omega_x$ ) contours on the WAKE 1 plane**

File name	fig3-06_00_nut.eps ( $\beta = 0^\circ$ , for $\nu_t$ ) fig3-06_06_nut.eps ( $\beta = 6^\circ$ , for $\nu_t$ ) fig3-06_12_nut.eps ( $\beta = 12^\circ$ , for $\nu_t$ ) fig3-06_00_omgx.eps ( $\beta = 0^\circ$ , for $\omega_x$ ) fig3-06_06_omgx.eps ( $\beta = 6^\circ$ , for $\omega_x$ ) fig3-06_12_omgx.eps ( $\beta = 12^\circ$ , for $\omega_x$ )
Axis size	160 [mm] $\times$ 40[mm]
Horizontal-axis variable and range	$-0.16 \leq y/L_{PP} \leq 0.16$
Vertical-axis variable and range	$-0.08 \leq z/L_{PP} \leq 0.0$
Contour levels	$\Delta\nu_t = 0.5 \times 10^{-5}$ , $\Delta\omega_x = 10$
Style	$\nu_t$ contours: solid lines $\omega_x$ contours: (+) solid lines; (-) dashed lines

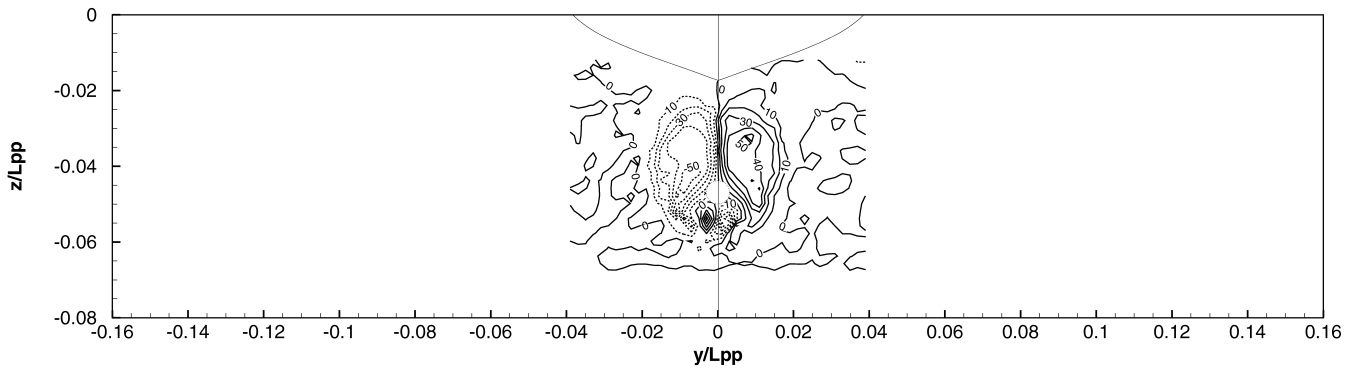


Fig. 3- 7: fig3-06\_00\_omgx.eps

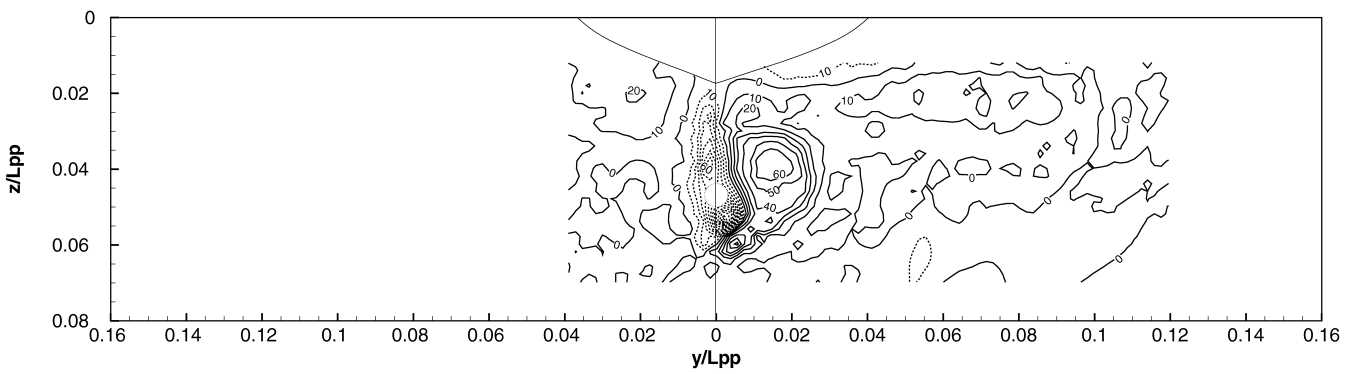


Fig. 3- 8: fig3-06\_06\_omgx.eps

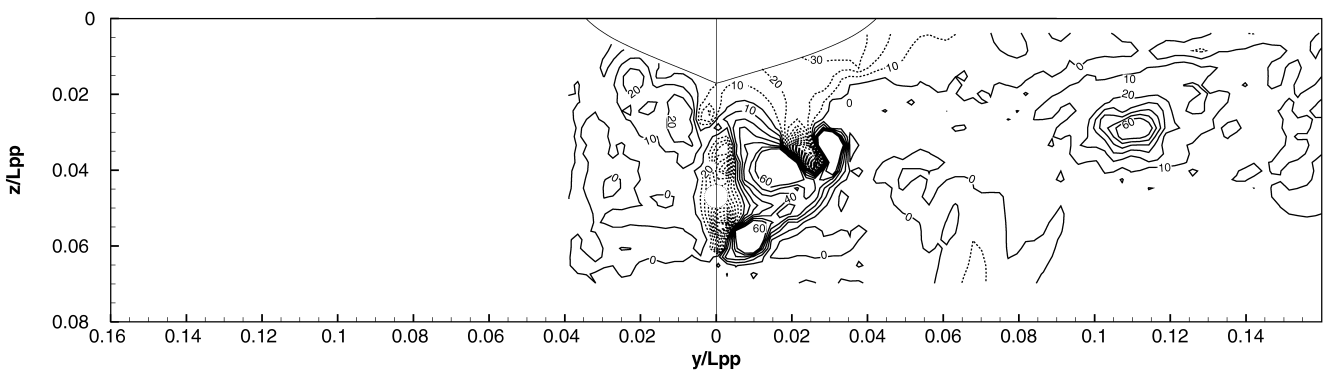


Fig. 3- 9: fig3-06\_12\_omgx.eps



**Fig.3-7 Hull surface pressure contours ( port side, starboard side, and bottom view )**

File name	fig3-07_06_fore.eps ( $\beta = 6^\circ$ , fore part ) fig3-07_06_aft.eps ( $\beta = 6^\circ$ , aft part ) fig3-07_12_fore.eps ( $\beta = 12^\circ$ , fore part ) fig3-07_12_aft.eps ( $\beta = 12^\circ$ , aft part )
Axis size	123.2 [mm] $\times$ 88 [mm]
Horizontal-axis variable and range	$-0.55 \leq x/L_{PP} \leq 0.0$ for fore part $0.0 \leq x/L_{PP} \leq 0.55$ for aft part
Vertical-axis variable and range	$-0.07 \leq z/L_{PP} \leq 0$ for port and starboard side view $-0.1 \leq y/L_{PP} \leq 0.1$ for bottom view
Contour range and levels	$-1.0 \leq C_p \leq 1.0$ , $\Delta C_p = 0.05$
Style	(+) solid lines; (-) dashed lines
Remarks	The order of arranging figures is port side view, bottom view, and starboard side view beginning at the top with proper spacing. The direction of $x$ axis is from left to right. The direction of $y$ axis in a bottom view and $z$ axis in a starboard side view are upside down.

**Fig.3-8 Hull surface pressure at  $x/L_{PP} = 0.4$  and  $x/L_{PP} = -0.4$** 

File name	fig3-08_00_s1.eps ( $\beta = 0^\circ$ , $x/L_{PP} = 0.4$ ) fig3-08_00_s9.eps ( $\beta = 0^\circ$ , $x/L_{PP} = -0.4$ ) fig3-08_06_s1.eps ( $\beta = 6^\circ$ , $x/L_{PP} = 0.4$ ) fig3-08_06_s9.eps ( $\beta = 6^\circ$ , $x/L_{PP} = -0.4$ ) fig3-08_12_s1.eps ( $\beta = 12^\circ$ , $x/L_{PP} = 0.4$ ) fig3-08_12_s9.eps ( $\beta = 12^\circ$ , $x/L_{PP} = -0.4$ )
Axis size	75 [mm] $\times$ 40 [mm]
Horizontal-axis variable and range	$-0.1 \leq y/L_{PP} \leq 0.1$
Vertical-axis variable and range	$-0.15 \leq C_p \leq 0.05$ , ( $\beta = 0^\circ$ , $x/L_{PP} = 0.4$ ) $-0.45 \leq C_p \leq 0.0$ , ( $\beta = 0^\circ$ , $x/L_{PP} = -0.4$ ) $-0.25 \leq C_p \leq 0.05$ , ( $\beta = 6^\circ$ , $x/L_{PP} = 0.4$ ) $-0.55 \leq C_p \leq 0.0$ , ( $\beta = 6^\circ$ , $x/L_{PP} = -0.4$ ) $-0.35 \leq C_p \leq 0.05$ , ( $\beta = 12^\circ$ , $x/L_{PP} = 0.4$ ) $-0.55 \leq C_p \leq 0.0$ , ( $\beta = 12^\circ$ , $x/L_{PP} = -0.4$ )
Style	CFD solid line, EFD open circles

**Red line** is corrected at 22/Dec/2004

NMRI-EXPERIMENT

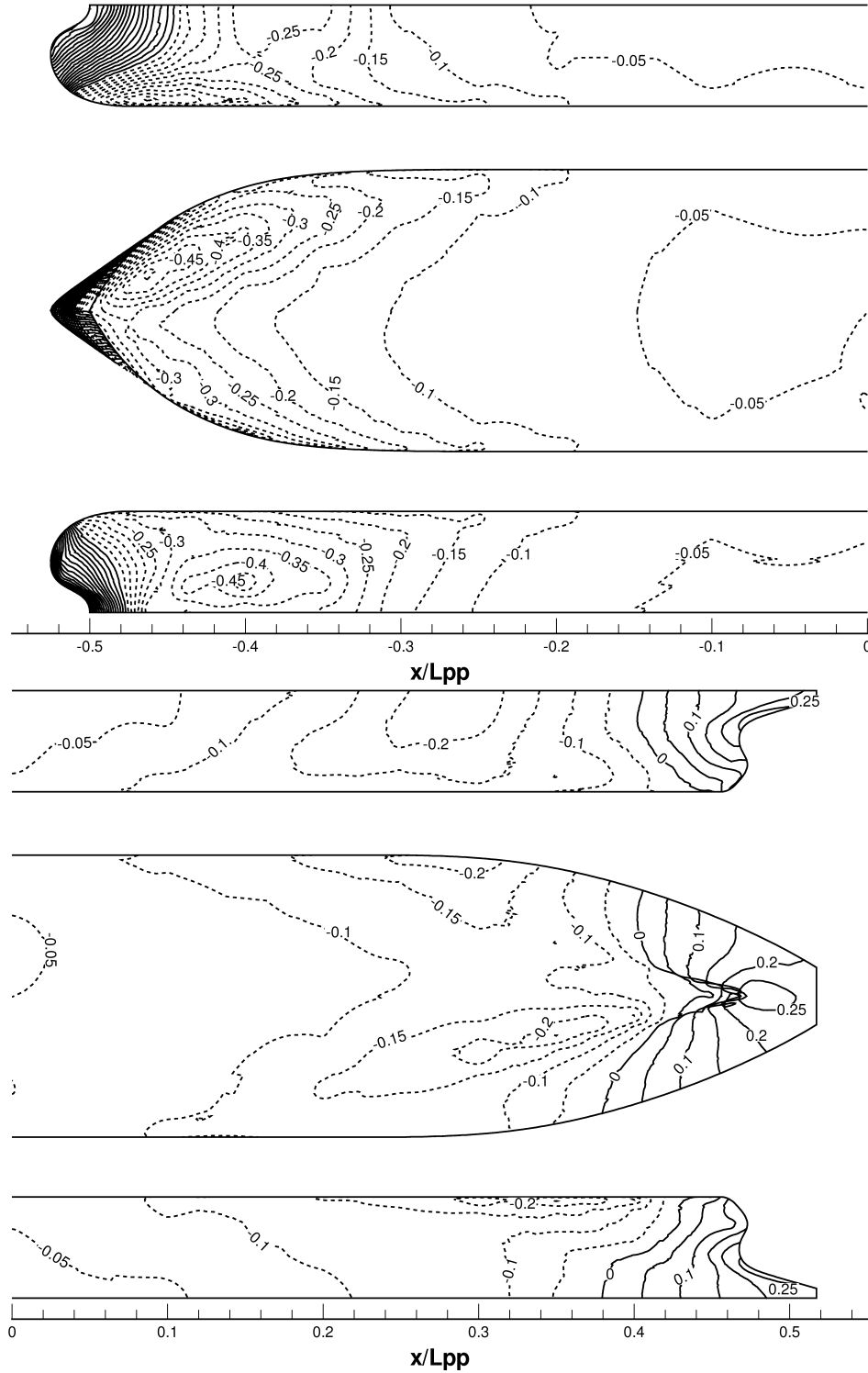


Fig. 3- 10: fig3-07\_06\_fore.eps (above) and fig3-07\_06\_aft.eps (below)

NMRI-EXPERIMENT

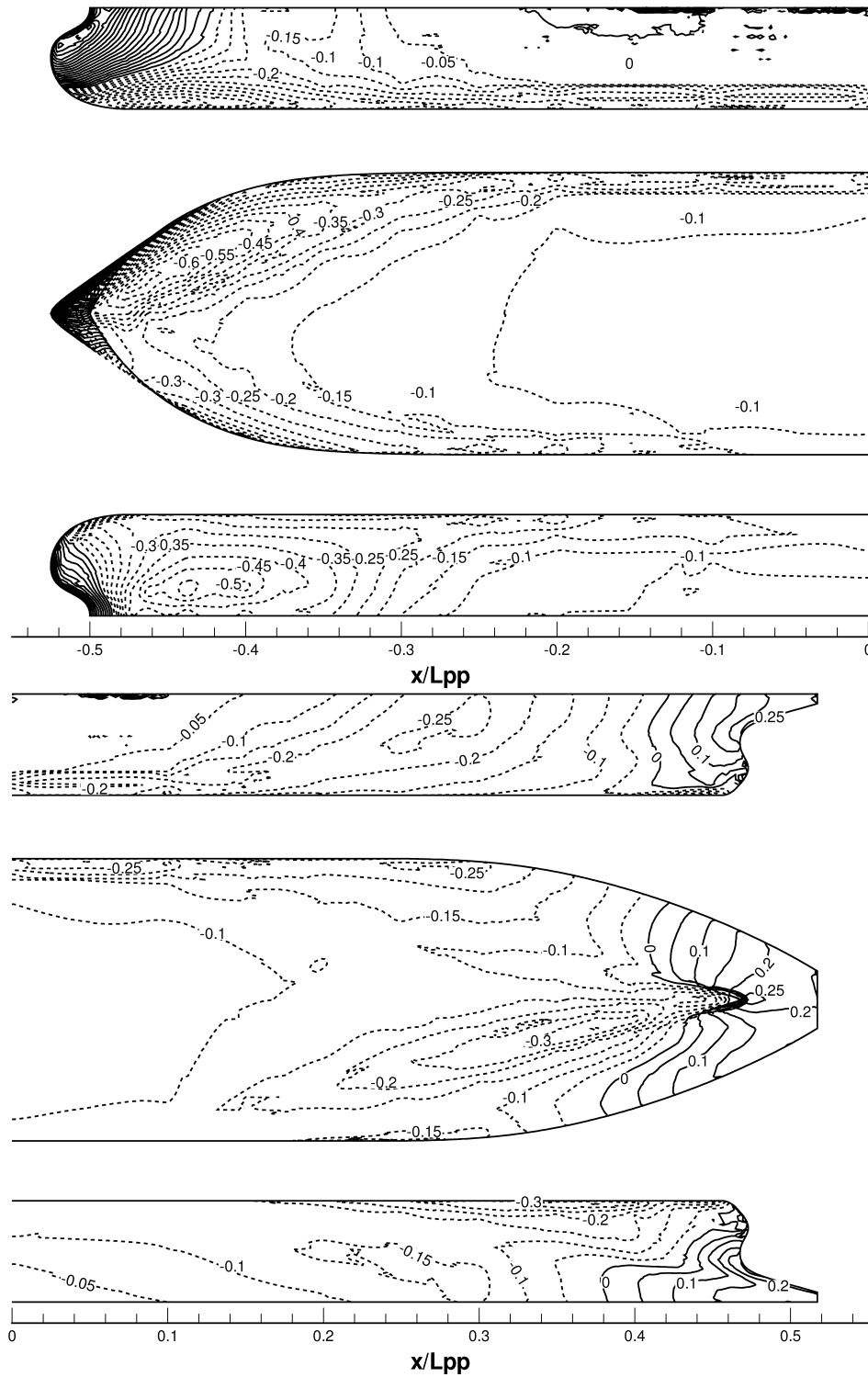


Fig. 3- 11: fig3-07\_12\_fore.eps (above) and fig3-07\_12\_aft.eps (below)

**Fig.3-9 Uncertainty analysis of hull surface pressure (  $U_{SN}, U_V, E$  )**  
**at  $x/L_{PP} = -0.4$  and  $x/L_{PP} = 0.4$**

File name	fig3-09_00_s1.eps ( $\beta = 0^\circ, x/L_{PP} = 0.4$ ) fig3-09_00_s9.eps ( $\beta = 0^\circ, x/L_{PP} = -0.4$ ) fig3-09_06_s1.eps ( $\beta = 6^\circ, x/L_{PP} = 0.4$ ) fig3-09_06_s9.eps ( $\beta = 6^\circ, x/L_{PP} = -0.4$ ) fig3-09_12_s1.eps ( $\beta = 12^\circ, x/L_{PP} = 0.4$ ) fig3-09_12_s9.eps ( $\beta = 12^\circ, x/L_{PP} = -0.4$ )
Axis size	80 [mm] $\times$ 60 [mm]
Horizontal-axis variable and range	$-0.1 \leq y/L_{PP} \leq 0.1$
Vertical-axis variable and range	$-0.6 \leq U_{SN}/C_{p\_range}, \pm U_V/C_{p\_range}, E/C_{p\_range} \leq 0.6$
Validation scale	$C_{p\_range} = 0.5, (\beta = 0^\circ, x/L_{PP} = 0.4)$ $C_{p\_range} = 0.1, (\beta = 0^\circ, x/L_{PP} = -0.4)$ $C_{p\_range} = 0.5, (\beta = 6^\circ, x/L_{PP} = 0.4)$ $C_{p\_range} = 0.2, (\beta = 6^\circ, x/L_{PP} = -0.4)$ $C_{p\_range} = 0.5, (\beta = 12^\circ, x/L_{PP} = 0.4)$ $C_{p\_range} = 0.3, (\beta = 12^\circ, x/L_{PP} = -0.4)$
Style	$\pm U_{SN}$ dotted line $U_V$ dashed line $E$ solid line

**Fig.3-10 Distribution of the side force component along the hull**

File name	fig3-10.06.eps ( $\beta = 6^\circ$ ) fig3-10.12.eps ( $\beta = 12^\circ$ )
Axis size	125 [mm] $\times$ 50 [mm]
Horizontal-axis variable and range	$-0.6 \leq x/L_{PP} \leq 0.6$
Vertical-axis variable and range	$-0.1 \leq \Delta Y_p \leq 0.5$
Style	CFD solid line, EFD open circles

**Red line** is corrected at 02/Dec/2004

### Fig.3-11 Uncertainty analysis of distribution of the side force component along the hull

File name	fig3-11.06.eps ( $\beta = 6^\circ$ ) fig3-11.12.eps ( $\beta = 12^\circ$ )
Axis size	125 [mm] $\times$ 50 [mm]
Horizontal-axis variable and range	$-0.6 \leq x/L_{PP} \leq 0.6$
Vertical-axis variable and range	$-0.6 \leq E/\Delta Y_{range}, \pm U_V/\Delta Y_{range} \leq 0.6$
Validation scale	$\Delta Y_{range} = 0.25$ ( $\beta = 6^\circ$ ) $\Delta Y_{range} = 0.5$ ( $\beta = 12^\circ$ )
Style	E solid line; $U_V$ dashed line

Red line is corrected at 02/Dec/2004

Magenta line is corrected at 28/Dec/2004

### Fig.3-12 Limiting stream lines ( port, starboard, and bottom views )

File name	fig3-12.06_fore.eps ( $\beta = 6^\circ$ , fore part ) fig3-12.06_aft.eps ( $\beta = 6^\circ$ , aft part ) fig3-12.12_fore.eps ( $\beta = 12^\circ$ , fore part ) fig3-12.12_aft.eps ( $\beta = 12^\circ$ , aft part )
Axis size	123.2 [mm] $\times$ 88 [mm]
Horizontal-axis variable and range	$-0.55 \leq x/L_{PP} \leq 0.0$ for fore part $0.0 \leq x/L_{PP} \leq 0.55$ for aft part
Vertical-axis variable and range	$-0.07 \leq z/L_{PP} \leq 0$ for port and starboard side view $-0.1 \leq y/L_{PP} \leq 0.1$ for bottom view
Style	Participants choose starting points and spacing
Remarks	The order of arranging figures is port side view, bottom view, and starboard side view beginning at the top with proper spacing. The direction of $x$ axis is from left to right. The direction of $y$ axis in a bottom view and $z$ axis in a starboard side view are upside down.

Red line is corrected at 08/Dec/2004

Magenta line is added at 18/Jan/2005